

**Problem 7.1.** Get as many analytical results as you possibly can for the temperature dependence of the phase-equilibrium pressure  $p_0(T)$  and the latent heat  $\Lambda(T)$  within the van der Waals model. In particular, explore the low-temperature limit ( $T \ll T_c$ ), and the close vicinity of the critical point  $\{P_c, V_c, T_c\}$ .

*Solution:*

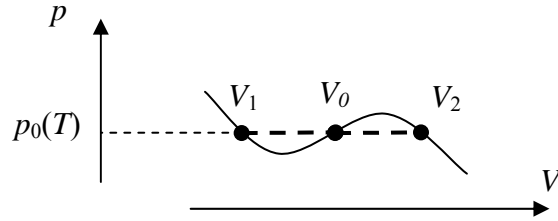
(a)  $T \approx T_c$ . Let us expand the van der Waals function

$$p(V, T) = \frac{NT}{V - Nb} - a \frac{N^2}{V^2} \quad (*)$$

into a Taylor series near the critical point

$$p_c = \frac{1}{27} \frac{a}{b^2}, \quad V_c = 3Nb, \quad T_c = \frac{8}{27} \frac{a}{b},$$

keeping only linear terms in  $T$ , but both the linear and cubic terms in  $V$ . (The last term is necessary to describe the hysteretic  $V(p)$  dependence:



pertinent for the 1<sup>st</sup> order phase transitions. Using normalized variables

$$\tilde{p} \equiv \frac{p - p_c}{p_c}, \quad \tilde{v} \equiv \frac{V - V_c}{V_c}, \quad \tilde{t} \equiv \frac{T - T_c}{T_c},$$

the series has the form

$$\tilde{p} = 4\tilde{t} - 6\tilde{t}\tilde{v} - \frac{3}{2}\tilde{v}^3. \quad (**)$$

Since this function is odd-symmetric in  $\tilde{v}$ , the phase equilibrium line  $p = p_0(T)$  (the dashed line in Fig. above) passes through the point  $\tilde{v} = 0$  (i.e.  $V_0 = V_c$ ), and

$$\tilde{p}_0 = 4\tilde{t}, \quad \text{i.e.} \quad p_0(T) = p_c - 4p_c \frac{T_c - T}{T_c}.$$

Because of the same symmetry, the end points  $V_{1,2}$  are on the equal distance from  $V_c$ :

$$V_2 - V_c = V_c - V_1 \equiv V_c \tilde{v}_0,$$

where according to Eq. (\*\*), at  $T < T_c$  ( $\tilde{t} < 0$ ):

$$-6\tilde{t}\tilde{v}_0 - \frac{3}{2}\tilde{v}_0^3 = 0, \quad \text{i.e.} \quad \tilde{v}_0 = 2\sqrt{-\tilde{t}},$$

so that

$$V_2 - V_1 = 2V_c\tilde{v}_0 = 4V_c\left(\frac{T_c - T}{T_c}\right)^{1/2}.$$

Now using the Clapeyron-Clausius formula, for the latent heat (per one particle) we get

$$\Lambda(T) = \frac{T}{N}(V_2 - V_1)\frac{dp_0}{dT} \approx \frac{T_c}{N}4V_c\left(\frac{T_c - T}{T_c}\right)^{1/2} \cdot 4\frac{p_c}{T_c} = 16\frac{p_c V_c}{N}\left(1 - \frac{T}{T_c}\right)^{1/2}.$$

(b)  $T \ll T_c$ . Let us start with writing down Maxwell's equal-area rule for  $p_0(T)$  in the following form:<sup>1</sup>

$$\int_{V_1}^{V_2} (p - p_0) dV = 0.$$

Plugging in the van der Waals equation (\*) for  $p$  and integrating, we get the following relation (valid, so far, for any temperature)

$$NT \ln \frac{V_2 - Nb}{V_1 - Nb} + aN^2 \left[ \frac{1}{V_2} - \frac{1}{V_1} \right] = p_0(V_2 - V_1). \quad (***)$$

In the limit  $T \rightarrow 0$ ,  $p_0(T)$  should tend to zero very fast, for the gas-phase Maxwell-rule area to be equal to the large liquid-phase area. (See, e.g., the numerical plot for  $T/T_c = 0.3$  on the next page.) As a result, the gas-phase volume  $V_2$  is much higher than not only the liquid-phase volume  $V_1 \approx Nb$ , but also the unstable-equilibrium volume  $V_0 \sim aN/T \gg Nb$  (at which both terms in the right-hand part of Eq. (\*) are comparable). Hence for the definition of  $V_2$  we can drop the terms with  $a$  and  $b$  in Eq. (\*), so that  $V_2$  is related to  $p_0$  by the ideal gas law:

$$p_0 = \frac{NT}{V_2},$$

Also, the difference  $V_1 - Nb$  is small and may be evaluated from Eq. (\*) with  $p \rightarrow 0$ :

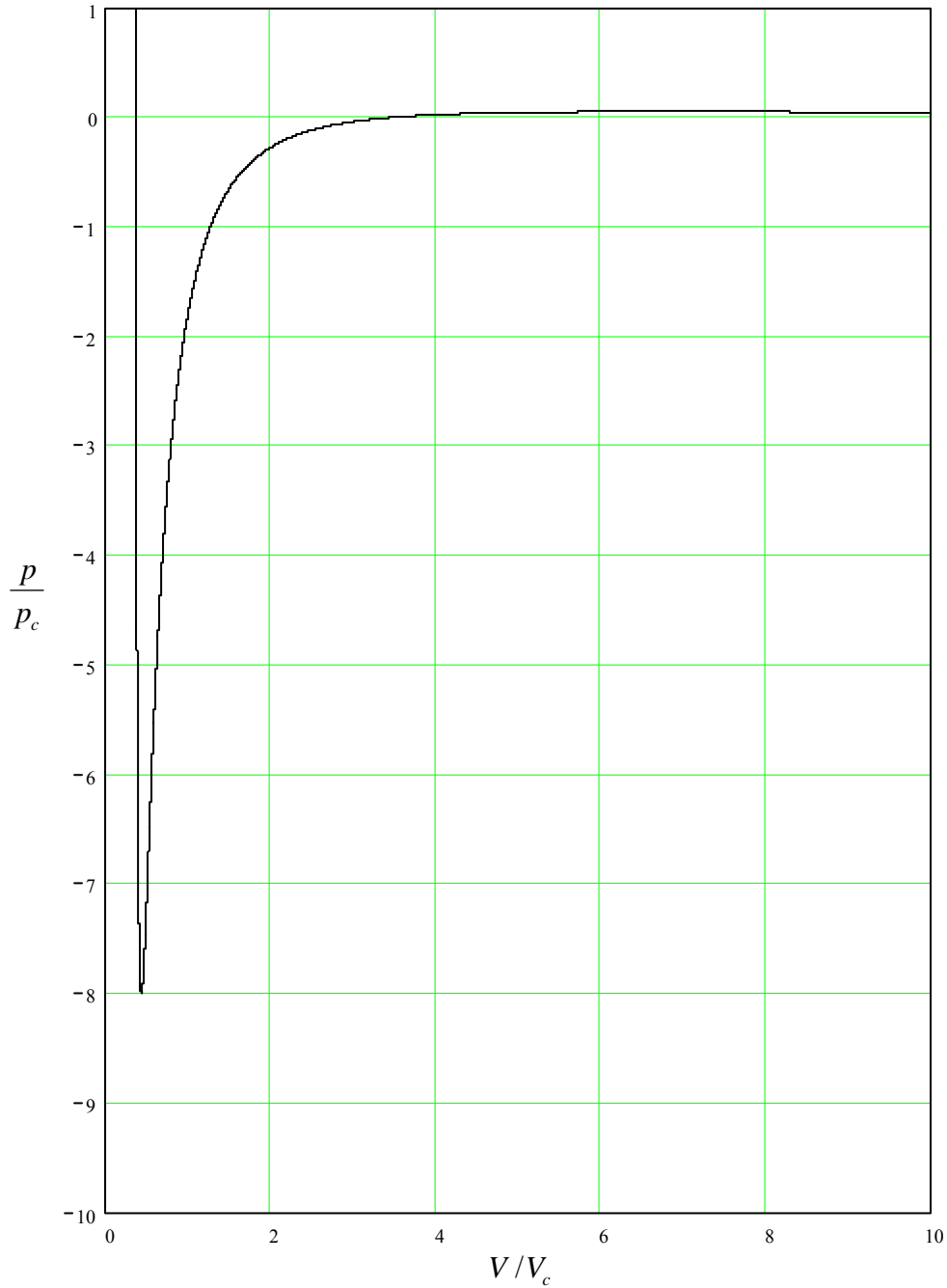
$$0 = \frac{NT}{V_1 - Nb} - a\frac{N^2}{(Nb)^2},$$

giving

$$V_1 = Nb + \frac{NTb^2}{a}.$$

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<sup>1</sup> In defining an area on a plane, the choice of integration direction is not important.



Plugging these relations into Eq. (\*\*\*) , we get a simple equation for  $V_2$ :

$$NT \ln \frac{aV_2}{NTb^2} - \frac{aN}{b} = NT,$$

which gives

$$V_2 = \frac{NTb^2}{a} \exp\left\{\frac{a}{b} + 1\right\} = \frac{NTb^2}{a} \exp\left\{\frac{27}{8} \frac{T_c}{T} + 1\right\} \approx \frac{NTb^2}{a} \exp\left\{\frac{27}{8} \frac{T_c}{T}\right\} \gg V_0, V_1,$$

thus justifying our assumptions. Finally, for the phase-equilibrium (the saturation vapor) pressure  $p_0$  we get

$$p_0(T) = \frac{NT}{V_2} = \frac{a}{b^2} \exp\left\{-\frac{27 T_c}{8 T}\right\} = 27 p_c \exp\left\{-\frac{27 T_c}{8 T}\right\} \ll p_c.$$

Note that the temperature dependence of  $p_0$  follows the exponential ‘‘Arrhenius’’ law (with the activation energy  $U = 27T_c/8$ ), in accordance with the basic physics of evaporation. (Physically,  $U$  is the molecular binding energy in the liquid phase.) It is amazing how well is this exponential law hidden inside the van der Waals equation of state (\*).

Now, using the Clapeyron-Clausius law, for the latent heat of evaporation (per molecule) we get a temperature-independent value

$$\Lambda(T) = \frac{T}{N}(V_2 - V_1) \frac{dp_0}{dT} \rightarrow \frac{T}{N} \frac{NTb^2}{a} \frac{27 T_c}{8 T^2} = \frac{27}{8} T_c = U,$$

which confirms the physical picture of evaporation, discussed in the last paragraph.